	8	OR			
9	Exp	plain with sketches the different types of	L2	CO1	10 M
	cam	as and followers.		CO3	
		UNIT-V			
10	a)	Derive natural frequency of free	L2	CO1	5 M
		longitudinal vibrations.		CO5	
	b)	A vibrating system consists of a mass of	L3	CO1	5 M
		200 kg, a spring of stiffness 80 N/mm		CO5	
		and a damper with damping coefficient of			
		800 N/m/s. Determine the frequency of			
		vibration of the system.			
		OR			
11	Ex	plain and Draw Turning moment diagram	L2	CO1	10 M
	of	steam engine.		CO4	

13

Code: 23ME3403

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# II B.Tech - II Semester - Regular Examinations - MAY 2025

# THEORY OF MACHINES (MECHANICAL ENGINEERING)

 Duration: 3 hours
 Max. Marks: 70

 Note: 1. This question paper contains two Parts A and B.
 2. Part-A contains 10 short answer questions. Each Question carries 2 Marks.

 3. Part-B contains 5 essay questions with an internal choice from each unit. Each Question carries 10 marks.
 4. All parts of Question paper must be answered in one place.

 BL – Blooms Level
 CO – Course Outcome

# PART – A

		BL	CO
1.a)	What is the degree of freedom of a mechanism?	L2	CO1
1.b)	Classify different types of constrained motion?	L2	C01
1.c)	What is the Coriolis component of acceleration?	L2	CO1 CO2
1.d)	State kennedy's theorem.	L1	CO2 CO1 CO2
1.e)	Explain about interference.	L2	CO1 CO3
1.f)	Explain about a Gear train.	L2	CO1 CO3
1.g)	Explain about Dynamic balancing.	L2	CO1 CO4
1.h)	What is pressure angle in Cam?	L2	C01 C04
1.i)	Explain about coefficient of fluctuation of energy.	L2	CO1 CO5
1.j)	What is damping coefficient?	L2	CO1 CO5

Page 1 of 4

**PVP 23** 

		PART – B			
			BL	со	Max. Marks
		UNIT-I			
2	a) Clas sket	ssify kinematic pairs with a neat ch.	L2	CO1	6 M
		tch any two inversions of single slider k chain.	L2	CO1	4 M
		OR			
3	-	lain any one of the approximate ght line mechanisms.	L2	CO1	5 M
	b) What used	at is a Hook's joint and where is it al?	L2	CO1	5 M
		UNIT-II			
4	In a four	L3	CO1	10 M	
	150 mm		CO2		
	and rota	tes at 120 r.p.m. clockwise, while the			
	link CD				
	AD are	of equal length. Calculate the angular			
	velocity	of link CD when angle $BAD = 60^{\circ}$			
	by instar	ntaneous center method.			
		OR			
5	For cont	figuration of slider-crank mechanism	L3	C01	10 M
	shown, c	calculate acceleration of Slider B.		CO2	
		450 A 480 60 5 (mm) G			
		Page 2 of 4			

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Page 2 of 4

		UNIT-III			
6	a)	Classify different types of gear trains.	L2	CO1 CO3	6 M
	1		TO		4 14
	b)	State law of gearing.	L2	CO1	4 M
				CO3	
		OR			
7	An	aeroplane flying at 240 km/hr turns	L3	CO1	10 M
	tow	ards the left and completes a quarter circle		CO4	
	of	50 m radius. The mass of the rotary engine			
	and	the propeller of the plane is 450 kg with a			
	rad	ius of gyration of 320 mm. The engine			
	spe	ed is 2000 rpm clockwise when viewed			
	from	n the rear. Determine the gyroscopic			
	cou	ple on the aircraft and state its effect.			
		•		11	
0	1.	UNIT-IV		COL	10.14
8		haft carries four masses A, B, C and D of	L3	CO1	10 M
	1	gnitude 200 kg, 300 kg, 400 kg and 200 kg		CO4	
	-	pectively and revolving at radii 80 mm,			
	1	mm, 60 mm and 80 mm in planes			
	mea	asured from A at 300 mm, 400 mm and			
	700	mm. The angles between the cranks			
	me	asured anticlockwise are A to B 45°, B to			
	C 7	$0^{\circ}$ and C to D 120°. The balancing masses			
	are	to be placed in planes X and Y. The			
	dist	ance between the planes A and X is 100			
	mm	h, between X and Y is 400 mm and			
	bet	ween Y and D is 200 mm. If the balancing			
	mas	sses revolve at a radius of 100 mm, find			
	the	r magnitudes and angular positions.			
-	1	Page 3 of 4		1	

# Code: 23ME3403

# II B.Tech-I Semester-Regular / Supplementary Examinations-

# May 2025

# **Theory of Machines**

# (MECHANICAL ENGINEERING)

# **Duration: 3 hours**

# Max. Marks: 70

Note: 1. This question paper contains Two Parts A and B

2. Part-A contains 10 short answer questions. Each question carries 2 Marks

3. Part-B contains 5 essay questions with an internal choice from each unit. Each question carries 10 Marks

# Answer the following questions.

# SCHEME OF EVALUATION

Question No	Concept to cover	BL	CO	Marks	Total Marks	
1.a)	Definition of degree of freedom of a mechanism	L2	1	1 Mark	2 Marks	
	example	1.1.6		1 Mark	2 Marks	
1.b)	Constrined motion types	L2	1	1 Mark	2 Marks	
	Names with example	1	100	1 Mark	- 2 Marks	
1.c)	Coriolis component of	L2	1,2	1 Mark		
	acceleration			1 Mark	2 Marks	
1.d)	Kennedy's theorem	L2	1,2	1 Mark	2 Marks	
edd all	equation			1 Mark		
1.e)	Interference with figure	L2	1,3	2 Marks	2 Marks	
1.f)	Gear train types	L2	1,3	2 Marks	2 Marks	
1.g)	Dynamic balancing explanation	L2	1,4	2 Marks	2 Marks	
1.h)	Pressure angel in cam definition and representation	L2	1,4	2 Marks	2 Marks	
1.i)	Definition of coefficient of fluctuation of energy	L2	1,5	2 Marks	2 Marks	
1.j)			1,5	2 Mark	2 Marks	
10 A A A	PAR	Т-В			1.	
	UNI	T-1				
2.a	Classification of kinematic pairs	L2	1	4 Mark		
	Neat sketch explanation	L2	1	2 Marks		
2.b	Inversions of single slider crank chain with neat sketch	L2	1	4 Marks	10 Marks	

1

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	OF	2				
3.a	Any type of approximate straight line mechanism with neat sketch	L2	1	5 Marks		
3.b	Hook's joint purpose and application	L2 1		5 Marks	10 Marks	
	UNIT	-II				
4.	Instantaneous method representation using the given details	L2	1,2	7 Marks	10 Marks	
	Calculation of angular velocity of link ĈD	L2	1,2	3 Marks	_	
	OR	1				
5.	Velocity and acceleration of given problem	L2	1,2	8 Marks	10 Marks	
	Acceleration of slider B	L2	1,2	2 Marks		
	UN	IT-III				
6. a.	Gear trains types	L2	1,3	2 Marks	10 10-1	
	Explanation of each-type	L2	1,3	4 Marks	– 10 Marks	
6.b	Law of gearing explanation and Figure representation	L2	1,3	4 Marks		
	OR	2				
7.	Representation of the problem with given data	L3	1,4	2 Marks		
	Determination of gyroscopic couple	L2	1,4	6 Marks	10 Marks	
	Explanation of couple effect in statement	L2	1,4	2 Marks		
	UNIT	-IV				
8.	Representation of masses with angle	L3	1,4	2 Marks		
	Determination of balancing mass	L3	1,4	4 Marks	10 Marks	
	Determination of position of balancing mass	L3	1,4	4 Marks		
	OR	L .				
9.	Different types of cams and followers	L2	1,3	5 Marks	· · · · ·	
	With figure explanation	L2	1,3	5 Marks	10 Marks	
	UNIT	`-V				
10. a )	Natural frequency definition under free longitudinal vibration	L2	1,5	5 Marks	10 Marks	
10.b)	Given problem data representation and natural	L3`	1,5	5 Marks		

	frequency formula and substitution				
	. (0)	R)			
11.	Turning moment diagram representation	L2	1,4	5 Marks	10 Marks
	And explanation of turning moment diagram of steam engine	L2	1,4	5 Marks	

Silver Silver

Code: 20ME3302

# II B.Tech-I Semester-Regular / Supplementary Examinations-

#### **DECEMBER 2023**

# MATERIAL SCIENCE AND METALLURGY

#### (MECHANICAL ENGINEERING)

#### **Duration: 3 hours**

Max. Marks: 70

Note: 1. This question paper contains Two Parts A and B

Part-A contains 10 short answer questions. Each question carries 2 Marks
 Part-B contains 5 essay questions with an internal choice from each unit. Each question carries 10 Marks

#### Answer the following questions.

#### PART-A

1. a) What is the degree of freedom of a mechanism? L2 CO1 2 Marks

**Ans)** The degree of freedom (DOF) of a mechanism, also known as its mobility, represents the number of independent parameters or inputs required to fully define the position or motion of a system

# 1.b) Classify different types of constrained motion L2 CO1 2 Marks

Ans) There are three types of constrained motions. They are listed below:

Completely Constrained Motion Partially or Successfully Constrained Motion Incompletely Constrained Motion Completely Constrained Motion Completely constrained motion is defined as the type of motion where the motion of the pair is limited to only one direction. Successfully Constrained Motion Partially or successfully constrained motion is the kind of motion that can be in more than one direction without the influence of any external force. Incompletely Constrained Motion Incompletely constrained motion is the type of motion where the motion between a pair can take place in more than just one direction.

#### 1.c) What is the Coriolis component of acceleration L2 CO1,2 2 Marks

**Ans**). The Coriolis component of acceleration is a tangential acceleration that arises when a point on one rotating link slides along another link

#### 1.d) what is the kennedy theorem L2 CO1,2 2 Marks

Ans) Kennedy's theorem, also known as the "Three Centers in Line Theorem" or the "Aronhold-Kennedy Theorem of Three Centers," states that if three bodies have relative motion, their three instantaneous centers of velocity are collinear

#### 1.e) Expalin about interference? L2 CO1, 3 2 Marks

Ans) Interference in gears occurs when the tooth tips of one gear contact the non-' involute portion of the mating gear, causing potential damage or failure

#### 1.f) Explain about a Gear train L2 CO1, 3 2 Marks

Ans) A gear train is a system of two or more gears that work together to transmit ` rotational motion and torque.

Types of Gear Trains: Simple Gear Train ompound Gear Train Epicyclic Gear Train Reverted Gear Train

#### 1.g) Explain about dynamic balancing L2 CO1, 4 2 Marks

Ans) Dynamic balancing is a process of balancing rotating machinery to reduce vibration and improve performance. It involves measuring and correcting unbalance in rotating parts while they are in motion, ensuring that forces and moments are distributed evenly around the axis of rotation

# 1. h) What is pressure angle in Cam? L2 CO1, 4 2 Marks

Ans) In cam mechanisms, the pressure angle is the angle between the normal to the pitch curve (or the cam profile) and the instantaneous direction of the follower's motion. This angle is crucial because it represents the steepness of the cam profile and varies with the follower's movement.

# 1.i) Explain about coeeficient of fluctuation of energy L2 CO1, 5 2 Marks

5

Ans) The coefficient of fluctuation of energy (CFE) is a measure of how much the energy of a system, like a flywheel, fluctuates during a cycle. It's calculated as the ratio of the maximum fluctuation of energy to the total work done per cycle.

# 1.j) What is damping coefficent? L2 CO1, 5

Ans) A damping coefficient, often denoted by "c," is a parameter that quantifies the amount of energy dissipation in a system due to damping forces, such as friction or air resistance

#### PART-B

# **UNIT-I**

# 2. a. Classify kinematic pairs with a neat sketch. L2, CO1 6M

# Ans)

#### Kinematic Pair:

A kinematic pair is a connection between two physical objects that imposes constraints on their relative movement.

The two links or elements of a machine, when in contact with each other, are said to form a pair. If the relative motion between them is completely or successfully constrained (i.e. in a definite direction), the pair is known as kinematic pair.

#### Types of kinematic pairs:

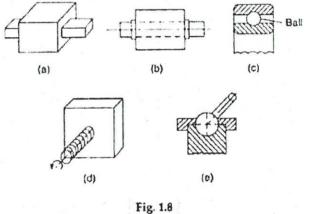
# Kinematic Pairs according to Nature of Relative Motion

(a) Sliding Pair If two links have a sliding motion relative to each other, they form a sliding pair.

A rectangular rod in a rectangular hole in a prism is a sliding pair [Fig. 1.8(a)].

(b) Turning Pair When one link has a turning or revolving motion relative to the other, they constitute a turning or revolving pair [Fig. 1.8(b)].

In a slider-crank mechanism, all pairs except the slider and guide pair are turning pairs. A circular shaft revolving inside a bearing is a turning pair.



(c) Rolling Pair When the links of a pair have a rolling motion relative to each other, they form a rolling pair, e.g., a rolling wheel on a flat surface, ball and roller bearings, etc. In a ball bearing [Fig. 1.8(c)], the ball and the shaft constitute one rolling pair whereas the ball and the bearing is the second rolling pair.

(d) Screw Pair (Helical Pair) If two mating links have a turning as well as sliding motion between them, they from a screw pair. This is achieved by cutting matching threads on the two links.

- The lead screw and the nut of a lathe is a screw pair [Fig. 1.8(d)].
- (e) Spherical Pair When one link in the form of a sphere turns inside a fixed link, it is a spherical pair. The ball and socket joint is a spherical pair [Fig. 1.8(c)].

#### Kinematic Pairs according to Nature of Contact

(a) Lower Pair A pair of links having surface or area contact between the members is known as a lower pair. The contact surfaces of the two links are similar.

Examples Nut turning on a screw, shaft rotating in a bearing, all pairs of a slider-crank mechanism, universal joint, etc.

(b) Higher Pair When a pair has a point or line contact between the links, it is known as a higher pair. The contact surfaces of the two links are dissimilar.

Examples Wheel rolling on a surface, cam and follower pair, tooth gears, ball and roller bearings, etc.

#### Kinematic Pairs according to Nature of Mechanical Constraint

(a) Closed Pair When the elements of a pair are held together mechanically, it is known as a closed pair.

Followe

Can

(a)

The two elements are geometrically identical; one is solid and full and the other is hollow or open. The latter not only envelops the former but also encloses it. The contact between the two can be broken only by destruction of at least one of the members.

All the lower pairs and some of the higher pairs are closed pairs. A cam and follower pair (higher pair) shown in Fig. 1.7(a) and a screw pair (lower pair) belong to the closed pair category.

(b) Unclosed Pair When two links of a pair are in contact either due to force of gravity or some spring action, they constitute an unclosed pair. In this, the links are not held together mechanically, e.g., cam and follower pair of Fig. 1.7(b).

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# 2.b) Sketch any two inversions of single slider crank chains.

#### L2 CO1 4M

Fig. 1.7

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(b)

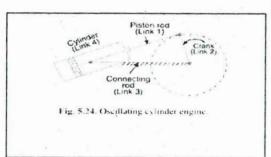
Follower

Cam

**1.** *Pendulum pump or Bull engine.* In this mechanism, the inversion is obtained by fixing the cylinder or link 4 (*i.e.*, sliding pair), as shown in Fig. 5.23. In this case, when the crank (link 2) rotates, the connecting rod (link 3) oscillates about a pin pivoted to the fixed link 4 at A and the piston attached to the piston rod (link 1) reciprocates. The duplex pump which is used to supply feed water to boilers have two pistons attached to link 1, as shown in Fig. 5.23.

7

2. Oscillating cylinder engine. The arrangement of oscillating cylinder engine mechanism, as shown in Fig. 5.24, is used to convert reciprocating motion into rotary motion. In this mechanism, the link 3 forming the turning pair is fixed. The link 3 corresponds to the connecting rod of a reciprocating steam engine mechanism. When the crank (link 2) rotates, the piston attached to piston rod (link 1) reciprocates and the cylinder (link 4) oscillates about a pin pivoted to the fixed link at A.



Piston rod (Link 4) Piston rod (Link 1) Crank (Link 2) Cylinder (Link 4) Fig. 5.23. Pendulum pump.

3. Rotary internal combustion engine or Gnome engine. Sometimes back, rotary internal combustion engines were used in aviation. But now-a-days gas turbines are used in its place. It consists of seven cylinders in one plane and all revolves about fixed centre D, as shown in Fig. 5.25, while the crank (link 2) is fixed. In this mechanism, when the connecting rod (link 4) rotates, the piston (link 3) reciprocates inside the cylinders forming link 1.

#### Note: Any two types are accepted

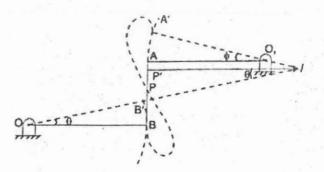
# OR

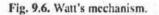
# 3. Explain any one of the approximate straight line mechanisms. L2, CO1 5M Ans)

8

The approximate straight line motion mechanisms are the modifications of the four-bar chain mechanisms. Following mechanisms to give approximate straight line motion, are important from the subject point of view :

1. Watt's mechanism. It is a crossed four bar chain mechanism and was used by Watt for his early steam engines to guide the piston rod in a cylinder to have an approximate straight line motion.





$$\operatorname{arc} B B' = \operatorname{arc} A A'$$
 or  $OB \times \theta = O_1 A \times \phi$  ...(i)

∴ Also

1

 $A'P' = IP' \times \phi$ , and  $B'P' = IP' \times \phi$ 

 $OBIO_1A = 0/0$ 

 $A'P' | B'P' = \phi / \theta$ 

From equations (i) and (ii),

OB	A'P'	AP		$\frac{O_1A}{=}$	PR
$\overline{O_1 A} =$	$\overline{B'P'}$ =	BP	or	$\frac{O_{11}}{OB} =$	

Thus, the point P divides the link A B into two parts whose lengths are inversely proportional to the lengths of the adjacent links.

#### Grasshopper Mechanism

In this mechanism, the centers O and O1 are fixed. The link OA oscillates about O
through an angle AOA1 which causes the pin P to move along a circular arc with
O1 as center and O1P as radius.

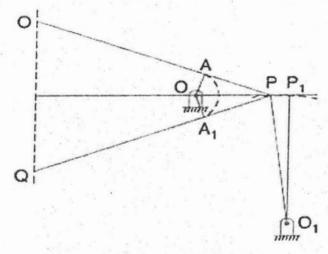


Fig. 2.7 Grasshopper Mechanism

For small angular displacements of OP on each side of the horizontal, the point Q
on the extension of the link PA traces out an approximately a straight path QQ'. if
the lengths are such that

. \* :

...(ii)

$$OA = \frac{AP^2}{AQ}$$

#### Note: any approximate straight line mechanism is accepted

## 3 b) What is a Hook's joint and where is it used? L2 CO1 5M

A Hooke's joint is used to connect two shafts, which are intersecting at a small angle, as shown in Fig. 9.18. The end of each shaft is forked to U-type and each fork provides two bearings

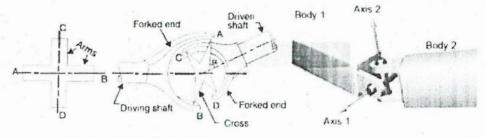


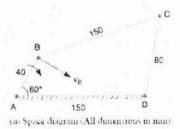
Fig. 9.18. Universal or Hooke's joint.

for the arms of a cross. The arms of the cross are perpendicular to each other. The motion is transmitted from the driving shaft to driven shaft through a cross. The inclination of the two shafts may be constant, but in actual practice it varies, when the motion is transmitted. The main application of the Universal or Hooke's joint is found in the transmission from the || gear box to the differential or back axle of the automobiles. It is also used for transmission of power to different spindles of multiple drilling machine. It is also used as a knee joint in milling machines.

#### **UNIT-II**

4. In a four bar chain ABCD, AD is fixed and is 150 mm long. The crank AB is 40mm long and rotates at 120 r.p.m. clockwise, while the link CD =80 mm oscillates about D. BC and AD are of equal length. Calculate the angular velocity of link CD when angle BAD =60 by instantaneous center method L2, CO2 10M

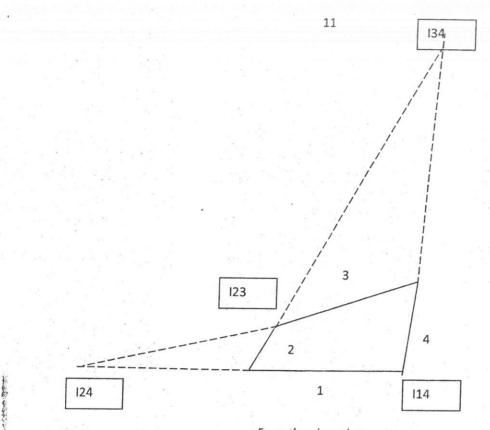
• Ans)



 $N_{\rm BA} = 120 \text{ r.p.m}$ 



10



From the given data:

- $AB = 40 \,\mathrm{mm}$
- BC = AD = 150 mm
- $CD = 80 \,\mathrm{mm}$
- $\angle BAD = 60^{\circ}$

Since AB is rotating at  $\omega_{AB}=4\pi\,\mathrm{rad/s}$ , the linear velocity of point B relative to A:

$$V_B = \omega_{AB} \times AB = 4\pi \times 40 = 160\pi \,\mathrm{mm/s} \approx 502.65 \,\mathrm{mm/s}$$

Direction of  $V_B$ : perpendicular to AB (due to pure rotation), clockwise.

- Link 1: Fixed (AD)
- Link 2: Crank AB
- Link 3: Coupler BC
- Link 4: CD

Finding Instantaneous Center  $I_{13}$ 

- I<sub>13</sub> lies at the intersection of:
  - The perpendicular to  $V_B$  at B (since B is on link AB, rotating)
  - The perpendicular to  $V_C$  at C (since C is on link CD, rotating)

We know from IC method:

$$\frac{V_B}{V_C} = \frac{I_{13}C}{I_{13}B}$$

But we can also write:

$$V_B = \omega_{BC} \times I_{13}B$$
$$V_C = \omega_{CD} \times CD$$

From velocity ratio:

$$rac{\omega_{BC} imes I_{13}B}{\omega_{CD} imes CD} = rac{I_{13}C}{I_{13}B} \Rightarrow \omega_{CD} = rac{\omega_{BC} imes I_{13}B^2}{CD imes I_{13}C}$$

This is complex algebraically, so we simplify by **applying geometry** to find the triangle positions when angle  $BAD = 60^{\circ}$ .

$$\frac{V_B}{V_C} = \frac{IC - C}{IC - B} \Rightarrow \frac{\omega_{AB} \cdot AB}{\omega_{CD} \cdot CD} = \frac{IC - C}{IC - B}$$

•  $IC - B = 100 \,\mathrm{mm}$ 

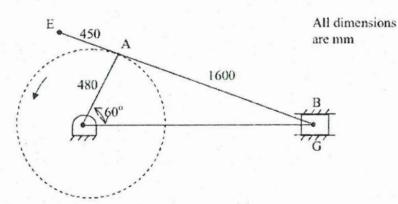
•  $IC - C = 60 \,\mathrm{mm}$ 

Then:

$$\frac{4\pi \cdot 40}{\omega_{CD} \cdot 80} = \frac{60}{100} \Rightarrow \omega_{CD} = \frac{4\pi \cdot 40 \cdot 100}{80 \cdot 60} = \frac{16000\pi}{4800} = \frac{100\pi}{30} \approx 10.47 \, \text{rad/s}$$

OR

5. For configuration of slider-crank mechanism shown, calculate acceleration slider B. L2, CO2 10M

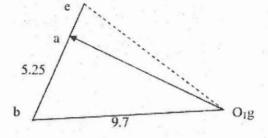


Step 1: Draw configuration diagram.

Step 2: Find velocity of A with respect to O.

 $V_a = \omega_{OA} \times OA$  $V_a = 20 \times 0.48$  $V_a = 9.6 \text{ m/s}$ 

Step 4: Draw velocity vector diagram.

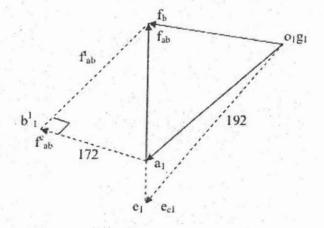


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Step 4:

SI. No.	Link	Magnitude	Direction	Sense
1.	OA	$f_{aO}^{c} = \omega_{OA}^{2} r = 192$	Parallel to OA	<b>→</b> 0
2.	AB	$f_{ab}^{c} = \omega_{ab}^{2} r = 17.2$ $f_{ab}^{c} = -$	Parallel to AB $\perp^t$ to AB	→ A
3.	Slider B	-	Parallel to Slider	

Step 5: Draw the acceleration diagram choosing a suitable scale.



- Mark o<sub>1</sub>g<sub>1</sub> (zero acceleration point)
- Draw  $\overline{o_1g_1} = C$  acceleration of OA towards 'O'.
- From  $a_1 draw a_1 b_1^1 = 17.2 \text{ m/s}^2$  towards 'A' from  $b_1^1 draw a line \perp^r$  to AB.
- From  $o_1g_1$  draw a line along the slider B to intersect previously drawn line at  $b_1$ ,  $\overrightarrow{a_1b_1} = f_{ab}$

 $\overline{g_1 b_1} = f_b = 72 \text{ m/s}^2$ .

• Extend 
$$\overline{a_1b_1} = \overline{a_1e_1}$$
 such that  $\frac{a_1b_1}{AB} = \frac{A_1R_1}{AE}$ 

o Join  $e_1$  to  $\delta_1 g_1$ ,  $g_1 e_1 = f_c = 236 \text{ m/s}^2$ .

$$\alpha_{ab} = \frac{f_{ab}^{1}}{AB} = \frac{b_{1}b_{1}}{AB} = \frac{167}{1.6} = 104 \text{ rad/sec}^{2} \text{ (CCW)}.$$

Answers:

 $f_b = 72 \text{ m/sec}^2$ 

# **UNIT-III**

# 6. Classift different types of gear trains L2, CO1-3 6 M

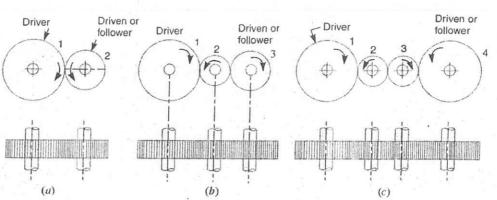
Following are the different types of gear trains, depending upon the arrangement of wheels :

1. Simple gear train, 2. Compound gear train, 3. Reverted gear train, and 4. Epicyclic gear train.

In the first three types of gear trains, the axes of the shafts over which the gears are mounted are fixed relative to each other. But in case of epicyclic gear trains, the axes of the shafts on which the gears are mounted may move relative to a fixed axis.

Simple Gear train:

When there is only one gear on each shaft, as shown in Fig. 13.1, it is known as *simple gear train*. The gears are represented by their pitch circles.

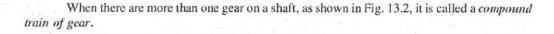


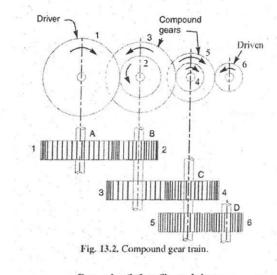
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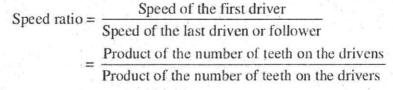
Fig. 13.1. Simple gear train.

$$\frac{N_1}{N_2} \times \frac{N_2}{N_3} = \frac{T_2}{T_1} \times \frac{T_3}{T_2} \quad \text{or} \quad \frac{N_1}{N_3} = \frac{T_3}{T_1}$$
Speed ratio =  $\frac{\text{Speed of driver}}{\text{Speed of driven}} = \frac{\text{No. of teeth on driven}}{\text{No. of teeth on driver}}$ 
Train value =  $\frac{\text{Speed of driven}}{\text{Speed of driver}} = \frac{\text{No. of teeth on driver}}{\text{No. of teeth on driver}}$ 

# Compound gear train:







### **Reverted Gear Train**

When the axes of the first gear (*i.e.* first driver) and the last gear (*i.e.* last driven or follower) are co-axial, then the gear train is known as *reverted gear* train as shown in Fig. 13.4.

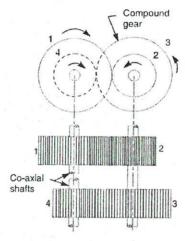


Fig. 13.4. Reverted gear train.

$$\frac{N_1}{N_4} = \frac{T_2 \times T_4}{T_1 \times T_3}$$

# **EpicyclicGearTrain**

We have already discussed that in an epicyclic gear train, the axes of the shafts, over which the gears are mounted, may move relative to a fixed axis. A simple epicyclic gear train is shown in Fig. 13.6, where a gear A and the arm C have a common axis at  $O_1$  about which they can rotate. The gear B meshes with gear A and has its axis on the arm at  $O_2$ , about which the gear B can rotate. If the

arm is fixed, the gear train is simple and gear A can drive gear B or vice-versa, but if gear A is fixed and the arm is rotated about the axis of gear A (*i.e.*  $O_1$ ), then the gear B is forced to rotate *upon* and *around* gear A. Such a motion is called epicyclic and the gear trains arranged in such a manner that one or more of their members move upon and around another member are known as *epicyclic gear trains* (*epi*, means upon and *cyclic* means around). The epicyclic gear trains may be simple or compound.

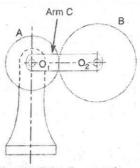


Fig. 13.6. Epicyclic gear train.

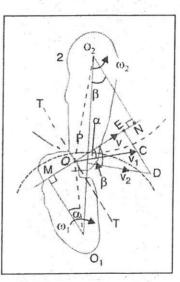
# 6. State law of gearing L2 CO1, CO3 4 Marks

Consider the portions of the two teeth, one on the wheel 1 (or pinion) and the other on the

wheel 2, as shown by thick line curves in Fig. 12.6. Let the two teeth come in contact at point Q, and the wheels rotate in the directions as shown in the figure.

Let T T be the common tangent and MN be the common normal to the curves at the point of contact Q. From the centres  $O_1$  and  $O_2$ , draw  $O_1M$  and  $O_2N$  perpendicular to MN. A little consideration will show that the point Q moves in the direction QC, when considered as a point on wheel 1, and in the direction QD when considered as a point on wheel 2.

Let  $v_1$  and  $v_2$  be the velocities of the point Q on the wheels 1 and 2 respectively. If the teeth are to remain in contact, then the components of these velocities along the common normal MN must be equal.



$$v_1 \cos \alpha = v_2 \cos \beta$$

or

...

$$\omega_{1} \times O_{1} Q) \cos \alpha = (\omega_{2} \times O_{2} Q) \cos \beta$$
  
$$\omega_{1} \times O_{1} Q) \frac{O_{1} M}{O_{1} Q} = (\omega_{2} \times O_{2} Q) \frac{O_{2} N}{O_{2} Q}$$

$$\frac{\omega_1}{\omega_2} = \frac{O_2 N}{O_1 M}$$

Also from similar triangles  $O_1MP$  and  $O_2NP$ .

$$\frac{O_2 N}{O_2 M} = \frac{O_2 P}{O_2 P}$$

Combining equations (i) and (ii), we have

$$\frac{\omega_1}{\omega_2} = \frac{O_2 N}{O_1 M} = \frac{O_2 P}{O_1 P}$$

or  $\omega_1 \times O_1 M = \omega_2 \times O_2 N$ 

...(i)

...(ii)

...(iii)

From above, we see that the angular velocity ratio is inversely proportional to the ratio of the distances of the point P from the centres  $O_1$  and  $O_2$ , or the common normal to the two surfaces at the point of contact Q intersects the line of centres at point P which divides the centre distance inversely as the ratio of angular velocities.

Therefore in order to have a constant angular velocity ratio for all positions of the wheels, the point *P* must be the fixed point (called pitch point) for the two wheels. In other words, *the common normal at the point of contact between a pair of teeth must always pass through the pitch point*. This is the fundamental condition which must be satisfied while designing the profiles for the teeth of gear wheels. It is also known as *law of gearing*.

#### OR

7. An aeroplane flying at 240 km/hr turns towards the left and completes a quarter circle of 60 m radius. The mass of the rotary engine and the propeller of the plane is 450 kg with a radius of gyration of 320 mm. The engine speed is 2000 rpm clockwise when viwered from the rear. Determine the gyroscopic couple on the airplane ands state its effect 13 *CO 1,4 10M* 

Given : R = 60 m ; v = 240 km/hr =  $\frac{240 \times 1000}{3600}$  = 66.67 m/s ; m = 450 kg ; k = 0.32 m

N = 2000 r.p.m. or  $\omega = 2\pi N/60 = 2\pi \times 2000/60 = 209.43$  rad/s

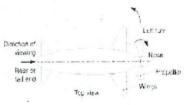
Mass moment of inertia of the rotor,  $I = m k^2 = 450 (0.32)^2 = 46.08 \text{ kg-m}^2$ 

Angular velocity of precession,  $\omega_p = \frac{v}{R} = \frac{66.67}{60} = 1.11$  rad/s

Gyroscopic couple,  $C = I \omega \omega_p = 46.08 \text{ x } 209.43 \text{ x } 1.11 = 10712.09 \text{ N-m}$ 

#### Effect

When the aero-plane turns towards left, the effect of the gyroscopic couple is to lift the nose upwards and tail downwards.



When the engine or propeller rotates in clockwise direction when viewed from the rear or tail end and the aeroplane takes a right turn, the effect of the reactive gyroscopic couple will be to dip the nose and raise the tail of the aeroplane.

#### **UNIT-IV**

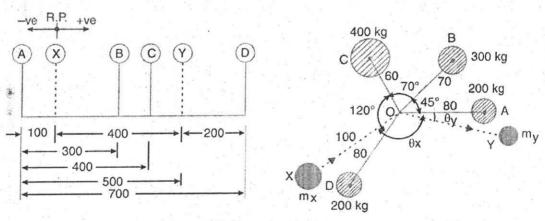
8. A shaft carries four masses A, B, C, and D with magnitudes 200 kg, 300 kg, 400 kg, and 200 kg respectively. They revolve at radii of 80 mm, 70 mm, 60 mm, and 80 mm in planes measured from A at 300 mm, 400 mm, and 700 mm. The angles between the cranks measured anticlockwise are A to B 45°, B to C 70°, and C to D 120°. Balancing masses are to be placed in planes X and Y. The distance between planes A and X is 100 mm, between X and Y is 400 mm, and between Y and D is 200 mm. If the balancing masses revolve at a radius of 100 mm, find their magnitude and angular positions. L3 CO 1,4 10 Marks

Solution. Given :  $m_A = 200 \text{ kg}$  ;  $m_B = 300 \text{ kg}$  ;  $m_C = 400 \text{ kg}$  ;  $m_D = 200 \text{ kg}$  ;  $r_A = 80 \text{ mm}$ = 0.08m ;  $r_B = 70 \text{ mm} = 0.07 \text{ m}$  ;  $r_C = 60 \text{ mm} = 0.06 \text{ m}$  ;  $r_D = 80 \text{ mm} = 0.08 \text{ m}$  ;  $r_X = r_Y = 100 \text{ mm}$ = 0.1 m

Let

 $m_{\rm X}$  = Balancing mass placed in plane X, and  $m_{\rm Y}$  = Balancing mass placed in plane Y.

Plane (1)	Mass (m) kg (2)	Radius (r) m (3)	Cent.force $\div \omega^2$ (m.r) kg-m (4)	Distance from Plane x(l) m (5)	Couple ÷ ω <sup>2</sup> (m.r.l) kg-m <sup>2</sup> (6)
<u>ল</u> A	200	0.08	16	- 0.1	- 1.6
X(R.P.)	m <sub>x</sub>	0.1	$0.1 m_{\rm X}$	0	0
B	300	0.07	21	0.2	4.2
C	400	0.06	24	0.3	7.2
Y	my	0.1	$0.1 m_y$	0.4	0.04 m <sub>Y</sub>
D	200	0.08	16	0.6	9.6

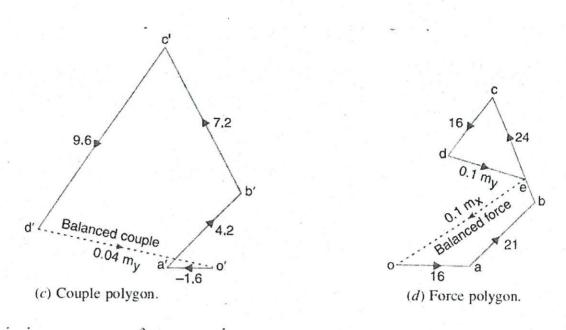


All dimensions in mm.

(a) Position of planes.

(b) Angular position of masses.

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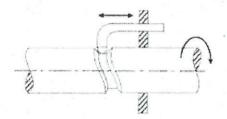


 $0.1 m_{\rm X} = \text{vector } eo = 35.5 \text{ kg-m}$  or  $m_{\rm X} = 355 \text{ kg Ans.}$ 

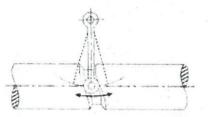
The angular position of the mass  $m_X$  is obtained by drawing  $Om_X$  in Fig. 21.8 (b), parallel to vector *eo*. By measurement, the angular position of  $m_X$  is  $\theta_X = 145^\circ$  in the clockwise direction from mass  $m_A$  (*i.e.* 200 kg). Ans.

# 9. Explain with sketches the different types of cams and followers L2, CO1-3 10M Classification of Cams

Though the cams may be classified in many ways; yet the following two types are important from the subject point of view :



(a) Cylindrical cam with reciprocating follower.



(b) Cylindrical cam with oscillating follower.

1. Radial or disc cam. In radial cams, the follower reciprocates or oscillates in a direction perpendicular to the cam axis. The cams as shown in Fig. 20.1 are all radial cams.

2. Cylindrical cam. In cylindrical cams, the follower reciprocates or oscillates in a direction parallel to the cam axis. The follower rides in a groove at its cylindrical surface. A cylindrical grooved cam with a reciprocating and an oscillating follower is shown in Fig. 20.2 (a) and (b) respectively.

#### **Classification of follower:**

The followers may be classified as discussed below :

<sup>2</sup> 1. According to the surface in contact. The followers, according to the surface in contact, are as follows :

- (a) Knife edge follower. When the contacting end of the follower has a sharp knife edge, it is called a knife edge follower, as shown in Fig. 20.1 (a). The sliding motion takes place between the contacting surfaces (*i.e.* the knife edge and the cam surface). It is seldom used in practice because the small area of contacting surface results in excessive wear. In knife edge followers, a considerable side thrust exists between the follower and the guide.
- (b) Roller follower. When the contacting end of the follower is a roller, it is called a roller follower, as shown in Fig. 20.1 (b). Since the rolling motion takes place between the contacting surfaces (*i.e.* the roller and the cam), therefore the rate of wear is greatly reduced. In roller followers also the side thrust exists between the follower and the guide. The roller followers are extensively used where more space is available such as in stationary gas and oil engines and aircraft engines.
- (c) Flat faced or mushroom follower. When the contacting end of the follower is a perfectly flat face, it is called a flat-faced follower, as shown in Fig. 20.1 (c). It may be noted that the side thrust between the follower and the guide is much reduced in case of flat faced followers. The only side thrust is due to friction between the contact surfaces of the follower and the cam. The relative motion between these surfaces is largely of sliding nature but wear may be reduced by off-setting the axis of the follower, as shown in Fig. 20.1 (f) so that when the cam rotates, the follower also rotates about its own axis. The flat faced followers are generally used where space is limited such as in cams which operate the values of automobile engines.

(d) Spherical faced follower. When the contacting end of the follower is of spherical shape, it is called a spherical faced follower, as shown in Fig. 20.1 (d). It may be noted that when a flat-faced follower is used in automobile engines, high surface stresses are produced. In order to minimise these stresses, the flat end of the follower is machined to a spherical shape.

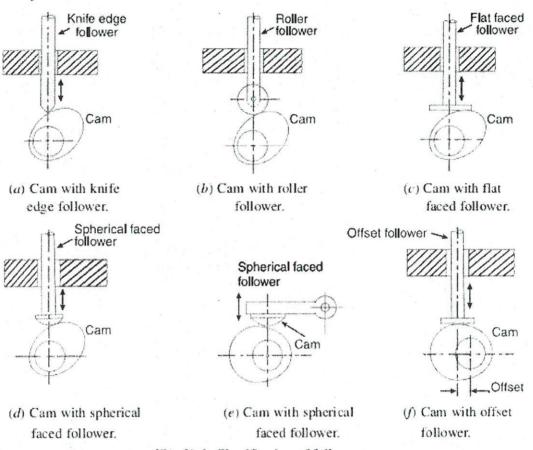


Fig. 20.1. Classification of followers.

2. According to the motion of the follower. The followers, according to its motion, are of the following two types:

- (a) Reciprocating or translating follower. When the follower reciprocates in guides as the cam rotates uniformly, it is known as reciprocating or translating follower. The followers as shown in Fig. 20.1 (a) to (d) are all reciprocating or translating followers.
- (b) Oscillating or rotating follower. When the uniform rotary motion of the cam is converted into predetermined oscillatory motion of the follower, it is called oscillating or rotating follower. The follower, as shown in Fig 20.1 (e), is an oscillating or rotating follower.

3. According to the path of motion of the follower. The followers, according to its path of motion, are of the following two types:

- (a) Radial follower. When the motion of the follower is along an axis passing through the centre of the cam, it is known as radial follower. The followers, as shown in Fig. 20.1 (a) to (e), are all radial followers.
- (b) Off-set follower. When the motion of the follower is along an axis away from the axis of the cam centre, it is called off-set follower. The follower, as shown in Fig. 20.1 (f), is an off-set follower.

#### UNIT-V

#### 10 a) Derive natural frequency of free longitudinal vibrations. L2 CO1, CO5 5 Marks

1. Free or natural vibrations. When no external force acts on the body, after giving it an initial displacement, then the body is said to be under free or natural vibrations. The frequency of the free vibrations is called free or natural frequency.

#### 3. Rayleigh's method

In this method, the maximum kinetic energy at the mean position is equal to the maximum potential energy (or strain energy) at the extreme position. Assuming the motion executed by the vibration to be simple harmonic, then

where

 $x = X \sin \omega t$ x = Displacement of the body from the mean position after time tseconds, and

X = Maximum displacement from mean position to extreme position.

Now, differentiating equation (i), we have

$$\frac{dx}{dt} = \omega \times X \cos \omega t$$

Since at the mean position, t = 0, therefore maximum velocity at the mean position,

$$v = \frac{dx}{dt} = \omega X$$

Maximum kinetic energy at mean position •

and maximum potential energy at the extreme position

$$=\left(\frac{0+s.X}{2}\right)X = \frac{1}{2} \times s.X^{2} \qquad \dots \quad (iii)$$

Equating equations (ii) and (iii),

$$\frac{1}{2} \times m \cdot \omega^2 \cdot X^2 = \frac{1}{2} \times s \cdot X^2 \quad \text{or} \quad \omega^2 = \frac{s}{m} \text{, and } \omega = \sqrt{\frac{s}{m}}$$
  
Time period,  $t_p = \frac{2\pi}{\omega} = 2\pi \sqrt{\frac{s}{m}}$  ... (Same as before)

 $f_n = \frac{1}{t_p} = \frac{\omega}{2\pi} = \frac{1}{2\pi} \sqrt{\frac{s}{m}}$ and natural frequency,

...

. . . (Same as before)

...(i)

Note : In all the above expressions, wis known as natural circular frequency and is generally denoted by ω".

#### UNIT-V

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10. B. A longitudinal system consists of a mass of 200 kg, a spring of stiffness 80 N/mm and a damper with damping coeeeficient of 800 N/m/s. Determine the frequency of vibration of the system.L3, CO1 5 5M

The natural frequency of a spring-mass system is given by,

$$f_n=rac{\omega_n}{2\pi}$$
 and  $\omega_n=\sqrt{rac{k}{m}}$ 

where k = spring stiffness (N/m) and m = mass of the body (kg)

#### Calculation:

#### Given:

Mass of body (m) = 200 kg, spring stiffness (k) = 80 N/mm =  $80 \times 10^3$  N/m

The natural frequency of vibration is:

$$\omega_n = \sqrt{\frac{k}{m}}$$
$$\omega_n = \sqrt{\frac{80 \times 10^3}{200}} = \sqrt{400} = 20 \ rad/s$$
OR

# 11. Explain and Draw Turning moment diagram of steam engine . L3, C05 10M

**Ans)** The turning moment diagram (also known as crankeffort diagram) is the graphical representation of the turning moment or crank-effort for various positions of the crank. It is plotted on cartesian co-ordinates, in which the turning moment is taken as the ordinate and crank angle as abscissa.

A turning moment diagram for a single cylinder double acting steam engine is shown in Fig. 16.1. The vertical ordinate represents the turning moment and the horizontal ordinate represents the crank angle.

We have discussed in Chapter 15 (Art. 15.10.) that the turning moment on the crankshaft,

$$T = F_{\rm P} \times r \left( \sin \theta + \frac{\sin 2\theta}{2\sqrt{n^2 - \sin^2 \theta}} \right)$$

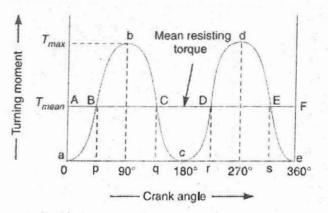


Fig. 16.1. Turning moment diagram for a single cylinder, double acting steam engine.

where

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- $F_{\rm P}$  = Piston effort,
- r =Radius of crank,
- n =Ratio of the connecting rod length and radius of crank, and
- $\theta$  = Angle turned by the crank from inner dead centre.

From the above expression, we see that the turning moment (T) is zero, when the crank angle ( $\theta$ ) is zero. It is maximum when the crank angle is 90° and it is again zero when crank angle is 180°. This is shown by the curve abc in Fig. 16.1 and it represents the turning moment diagram for outstroke. The curve cde is the turning moment diagram for instroke and is somewhat similar to the curve abc. Since the work done is the product of the turning moment and the angle turned, therefore the area of the turning moment diagram represents the work done per revolution. In actual practice, the engine is assumed to work against the mean resisting torque, as shown by a horizontal line AF. The height of the ordinate aA represents the mean height of the turning moment per revolution is equal to the work done against the mean resisting torque, therefore the area of the rectangle aAFe is proportional to the work done against the mean resisting torque.

e e